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INTERSTATE COUNCIL FOR STANDARDIZATION, METROLOGY AND CERTIFICATION  
(ISC)

**IEC**  
**62282-3-201—**  
**2015**

**3-201**

,

**(IEC 62282-3-201:2013, IDT)**



2016

IEC 62282-3-201—2015

,  
 1.0—2015 «  
 » 1.2—2015 «  
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 ( 27 2015 . 81- ).  
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 IEC 62282-3-201—2015  
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 1 2017 .

5 IEC 62282-3-201:2013 « 3-201.

» («Fuel cell technologies — Part 3-201: Stationary fuel cell power systems — Performance test methods for small fuel cell power systems», IDT).

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« \_\_\_\_\_ ».  
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( \_\_\_\_\_ )  
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IEC 62282-3-201:2013 «  
3-201.

Part 3-201: Stationary fuel cell power systems — Performance test methods for small fuel cell power systems»).  
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IEC 62282 «

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(<http://webstore.iec.ch>)

IEC 62282-3-201:2013 «

3-201.

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029 «

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» ( 010/2011).

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( 10 )

IEC 62282-3-200,

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3-201

Fuel cell technologies. Part 3-201. Stationary fuel cell power systems.  
Performance test methods for small fuel cell power systems

— 2017—05—01

**1**

/ -

- a) , : 10 ;  
b) : ;  
- ;  
- ;  
- ;  
- 1000 ;  
- 1500 ;  
— 1000 ,  
IEV 601-01-26.  
c) ; 0.1 ( )  
d) : ( , , . .);  
e) : , , , , , , . .);  
— ,  
— ,  
— ,  
— ,

**2**

(  
 IEC 62282-1, Electroacoustics — Sound level meters — Part 1: Specifications ( )  
 1.  
 IEC 62282-3-200, Fuel cell technologies — Part 3-200: Stationary fuel cell power systems—Performance test methods ( )  
 3-200.  
 ISO 5815 (all parts). Water quality — Determination of biochemical oxygen demand after n days (BOD<sub>n</sub>) (( ))  
 ISO 6060. Water quality — Determination of the chemical oxygen demand ( )  
 ISO 6798, Reciprocating internal combustion engines — Measurement of emitted airborne noise — Engineering method and survey method ( )  
 ISO 9000, Quality management systems — Fundamentals and vocabulary ( )  
 ISO 10523, Water quality — Determination of pH (pH)  
 ASTM F2602, Standard Test Method for Determining the Molar Mass of Chitosan and Chitosan Salts by Size Exclusion Chromatography with Multi-angle Light Scattering Detection (SEC-MALS) ( )  
 )

**3**

3.1 (noise level):

—  
15.2

( )

3.2 (background noise level):

—

3.3 (battery):

/

—

3.4 (cold state):  
(3.49),— IEC/TS 62282-1:2010,  
« »

3.110.1

3.5 (discharge rate):

- 3.6 (discharge water): ,  
—
- 3.7 (electric efficiency): ,  
,
- /TS, 3.30.1 :  
3.8 (electric energy input):  
3.9 (electric energy output):  
3.10 (electric power input):  
3.11 (electric power output):  
3.12 (fuel cell power system):  
3.13 , (fuel input): , ,  
,
- 3.14 (fuel power input): ,  
( )  
3.15 (heat recovery efficiency): ,  
,
- /TS 62282-1:2010, 3.30.3 :  
3.16 (heat recovery fluid): ,  
3.17 (inert purge gas): ,  
—  
3.18 (integrated fuel input): ,  
3.19 (interface point): /  
1 ( 2),  
2 62282-1:2010, 3.65.  
3.20 (mass concentration):  
3.21 (minimum electric power output): ,

IEC 62282-3-201—2015

- 3.22 (net electric power):
- 3.23 (nominal electric power):
- IEC/TS 62282-1:2010, 3.85.4
- 3.24 (overall energy efficiency):
- 3.25 (parasitic load):
- 3.26 (recovered heat of fuel cell power system):
- ( ), ( ), ( ).
- 3.27 (recovered thermal power):
- 3.28 (shutdown energy): / ( ),
- 3.29 (shutdown time): , , ,
- IEC/TS 62282-1:2010, 3.115.4
- 3.30 (pre-generation state):
- IEC/TS 62282-1:2010, 3.110.4
- 3.31 (start-up energy): /
- a) ( ), ; , — , — /
- b) ( ), , — , — /
- 3.32 (start-up time):
- a) , — , ; , — , — ,
- b) , — , — , — ,
- IEC/TS 62282-1:2010, 3.115.5
- 3.33 (stationary fuel cell power system):
- IEC/TS 62282-1:2010, 3.49.3.
- 3.34 (storage state):

/

— IECfTS 62282-1:2010, 3.110.6 —

3.35 (test run): ,

3.36 (thermal storage unit): ,

1

2

3.37 (waste heat): ,

3.38 (water consumption): , ( ) ,

**4**

/

1,

— 2.

1 — /

Qvf		3/
9vf0		3/
Qiv		3
Qvr		3/
<?ivHR		3
flvHR		3/
m <sub>0</sub>	( 2,3645 10 <sup>-2</sup> 3/ )	3/
^mf		/
^mHR		/
^imf		
<7imHR		
M		/
p <sub>nom</sub>		

instore		
^mm		
		/
		/
	^min	
Po	[101,325 ( .)]	( .)
Pf		( .)
f0	(288,15 )	
ff		
*HR1		-
*HR2		-
^HR	t <sub>HR1</sub>	/ <sup>3</sup>
Qfo		/
Qfl		/
O»i	j	Iq
S <sub>HR</sub>	f <sub>HR1</sub> f <sub>HR2</sub>	"1 "1
Qhr		/
E*	,	/ <sup>3</sup>
	,	/
Qinf		/
	,	
^instartubat	,	-
	,	-
W <sub>in</sub>	,	
^nshutdown	,	-
y <sup>/</sup> inst startup	,	-
Arista rtupbat	,	-
	TS <sub>1</sub>	-
TS <sup>^</sup> ,		-
^nbat	,	-
	TS <sub>1</sub>	-
rs <sub>3bat</sub>		-
Woutbat	,	-
	TS <sub>1</sub>	-
rs <sub>3bat</sub>		-

# 1

^instore	,	-
%		%
'/th		%
'/total		%
AT		
ATE		
7"lcdwn	$T_{te1}$   $z$	
	^ ) 4	
1 2	$\pm 2\%$	
^1		
4	$\pm 2\%.$	
ATS		
TS,		
rs <sub>2</sub>		
^3bat		
,	— ,	1.



«&gt; %ut



9mf



1 —

2 —

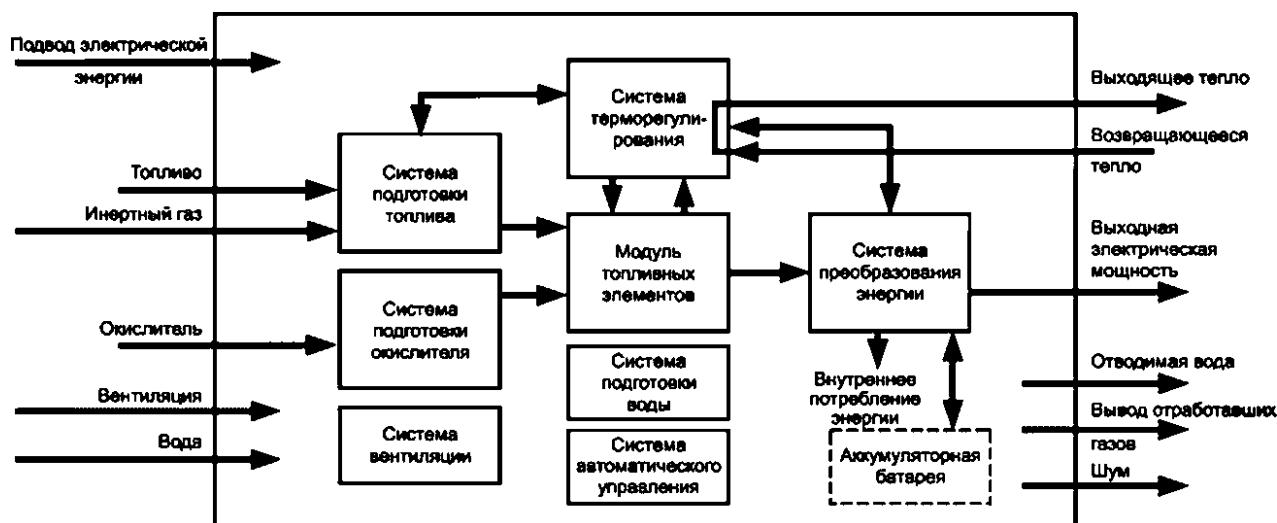
		. %, / <sup>3</sup> (ppm)
		% / <sup>3</sup> (ppm)
O <sub>2t</sub>	( <sup>2</sup> = 21 %)	.%
<sub>2</sub>	<sup>2</sup>	. %
v <sub>f0</sub>		<sup>3/</sup>
		<sup>3/</sup>
	(288,15 )	
<		
	[101,325 ( .)]	( .)
P <sub>t</sub>	( )	( .)
4f		/
0	( <sup>2,3645 - 10~2</sup> l <sub>q</sub> = 288,15 )	<sup>3/</sup>
		/
C <sub>Hat</sub>		
a <sub>f</sub>		
CO <sub>2dr</sub>	<sup>2</sup>	.%
<sub>2</sub>	44,01 ( <sub>2</sub> )	
<sup>^o2mass</sup>	<sup>2</sup>	/
*		<sup>3/</sup> (ppm)
	28,01 ( )	
<sup>^^mass</sup>		/
COconc		/ <sup>3</sup>
<sup>TM</sup>	( )	<sup>3/</sup> (ppm)
«		
TM		/
TM 0		/ <sup>3</sup>
WO <sub>Kdr</sub>	NOx	<sup>3/</sup> (ppm)
WO <sub>xM</sub>	46,61 ( NOx NO <sub>2</sub> ) , NOx	
A <sup>^xmass</sup>	NOx	/
w <sub>oxconc</sub>	NO <sub>x</sub>	/ <sup>3</sup>

2

SO <sub>2g,r</sub>	SO <sub>2</sub>	/ <sup>3</sup> (ppm)
SO <sub>2M</sub>	64,06 ( SO <sub>2</sub> )	
S <sup>mass</sup>	SO <sub>2</sub>	/
S <sup>2conc</sup>	SO <sub>2</sub>	/ <sup>3</sup>

5

2



2 —

6

- :  $I_0 = 288,15 \text{ (15 }^\circ\text{C)}$ ;  
- :  $I_0 = 101,325, \text{ ( )}$ .

7

(LHV).  
(LHV)  
«LHV»

$>I_e \cdot 'lthunu' total = \text{ % }$

IEC 62282-3-201—2015

(HHV),  
«HHV»:

/  $un_u_{lto_9}=XX\%(HHV)$ .

## 8

### 8.1

- a) ;
- b) ;
- c) ;
- d) (ISO 9000 , );
- e) ( 10);
- ) ;
- h)

### 8.2

— A IEC 62282-3-200:2011.

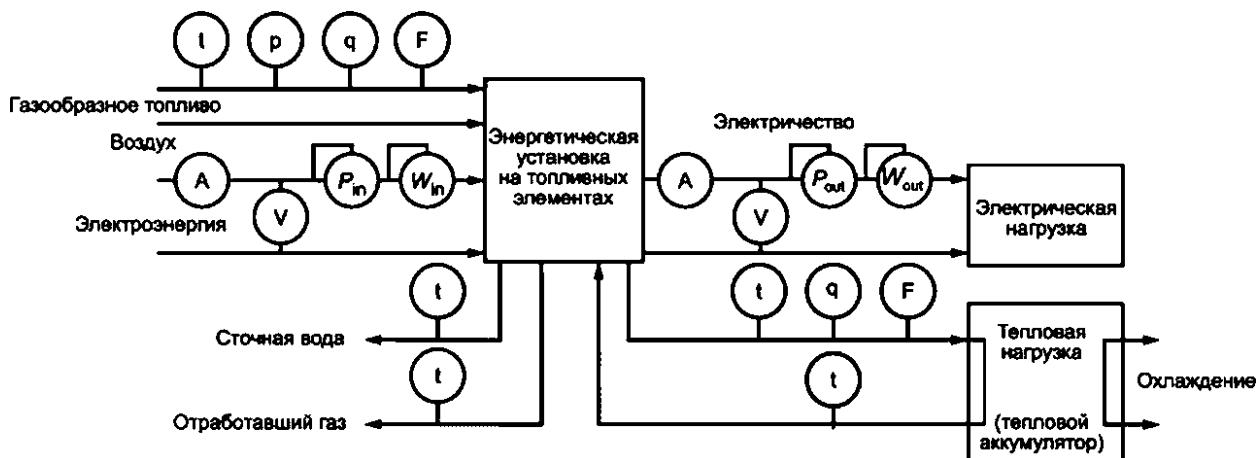
### 8.3

## 9

3

4

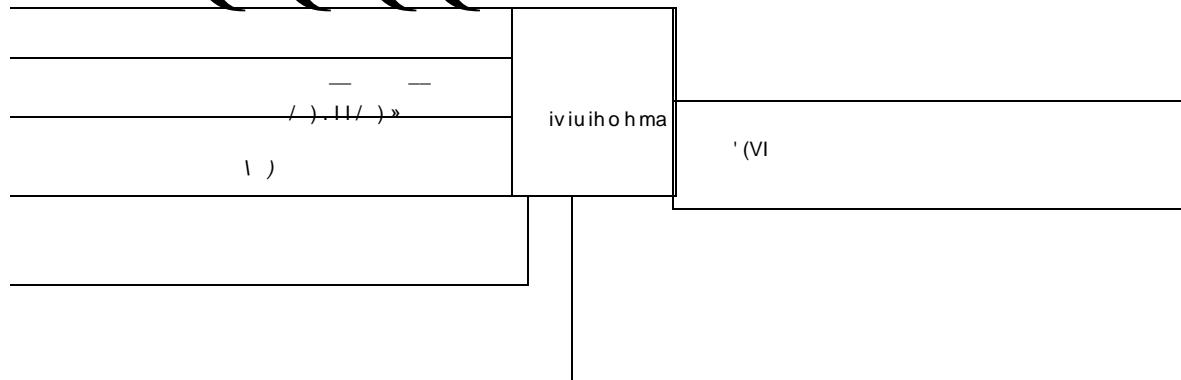
3



3 —

4.

Q Q QQ



— ; V — ; t — ( — ; q — ; F — ( );  
 $pH, , ;$

4 —

**10**

10.1

10.2

) , , , ( , ,  
 $;$   
 $, , , );$

- b),  
c),  
d),  
e);
- IEC 61672-1,
- ;
- - - : S;
- - - ( );
- 1) - - - ( );  
- - - ( );  
- - - ( );  
- - - ( );  
- - - ( );  
- - - ( );  
- - - ( );  
- ) , pH-, ( ).
- «» — «»

10.3

- a)
- b)
- c)
- d)
- f)
- g)
- h)
- i)
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;
- ;

- j) ; ,
- k) ( -  
): ( ), -  
;
- l) ( ); ( ): -  
( ), -  
;
- m) ( ); ( ): -  
;
- n) ( ); ( ): -  
;
- o) ( ); ( ): -  
;
- p) 4.186 "1 -1; : ,  
;
- q) , ;  
)
- r) ; ;  
;
- s) : 15.2.2;  
t) : ,  
,
- u) ( 3); : ,  
)
- v) 10.4 ,  
;
- w) 3 %  
2 % ,  
;
- x) : ± 1 %;  
: ± 1 %;  
: ± 1 %;  
: ± 1 %;  
: ± 1 %;  
: ± 1 %;  
: ± 0,5 %;  
: ± 1 %; : ± 2 %  $Af = f_{HR1} - f_{HR2}$ ;

- :  $\pm 5\%$ ;
- :  $\pm 1\%$ ;
- :  $\pm 1\%$ ;
- :  $\pm 4\%$ .

**11**

## 11.1

- ,
- :
- :  $(20 \pm 15)^\circ\text{C}$ ;
- :  $(65 \pm 20)\%$ ;
- : 91 ( ) 106 ( ).

(  $\text{O}_2$  ,  $\text{SO}_2$  . . )

## 11.2

## 11.3

a)

b)

(14.5.1).

## 11.4

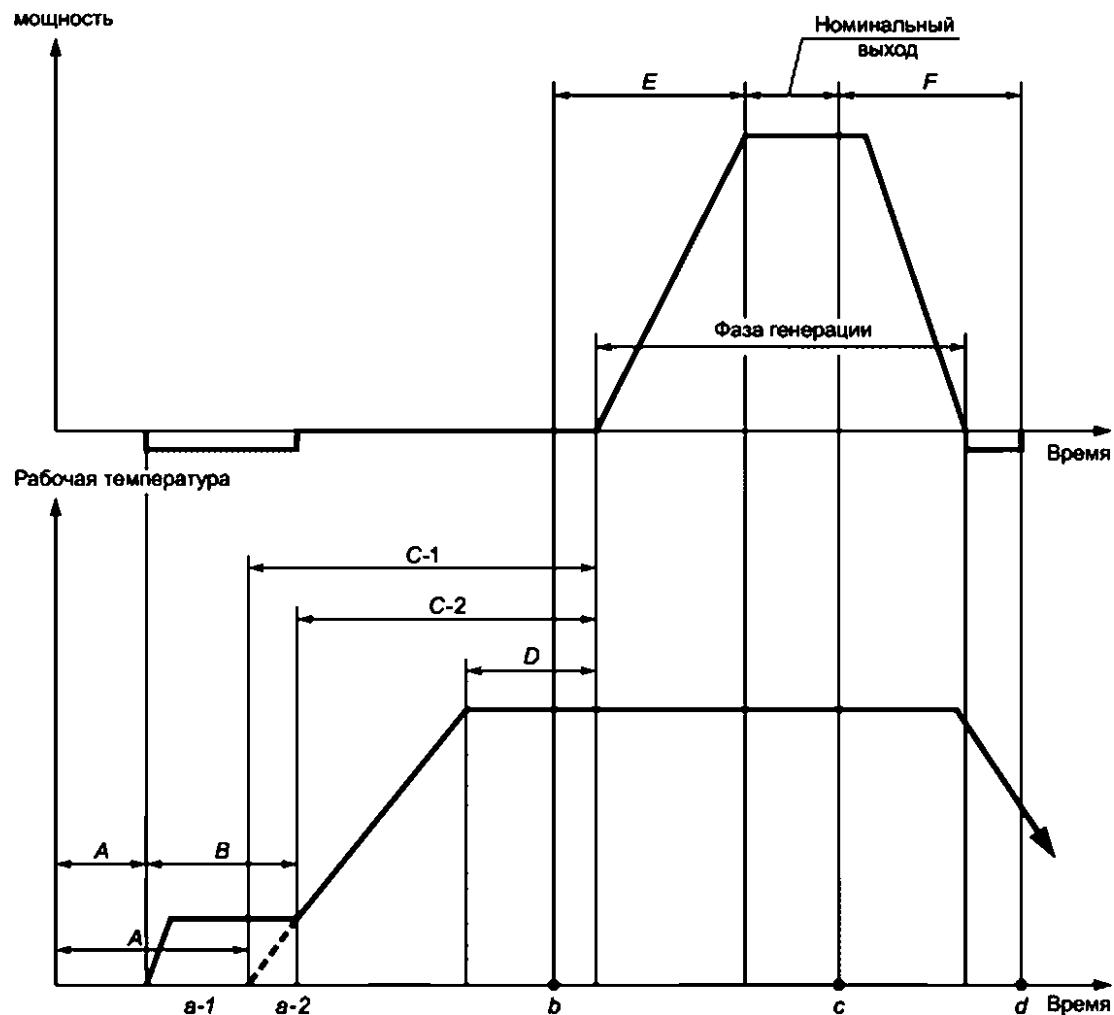
.1 .2

**12**

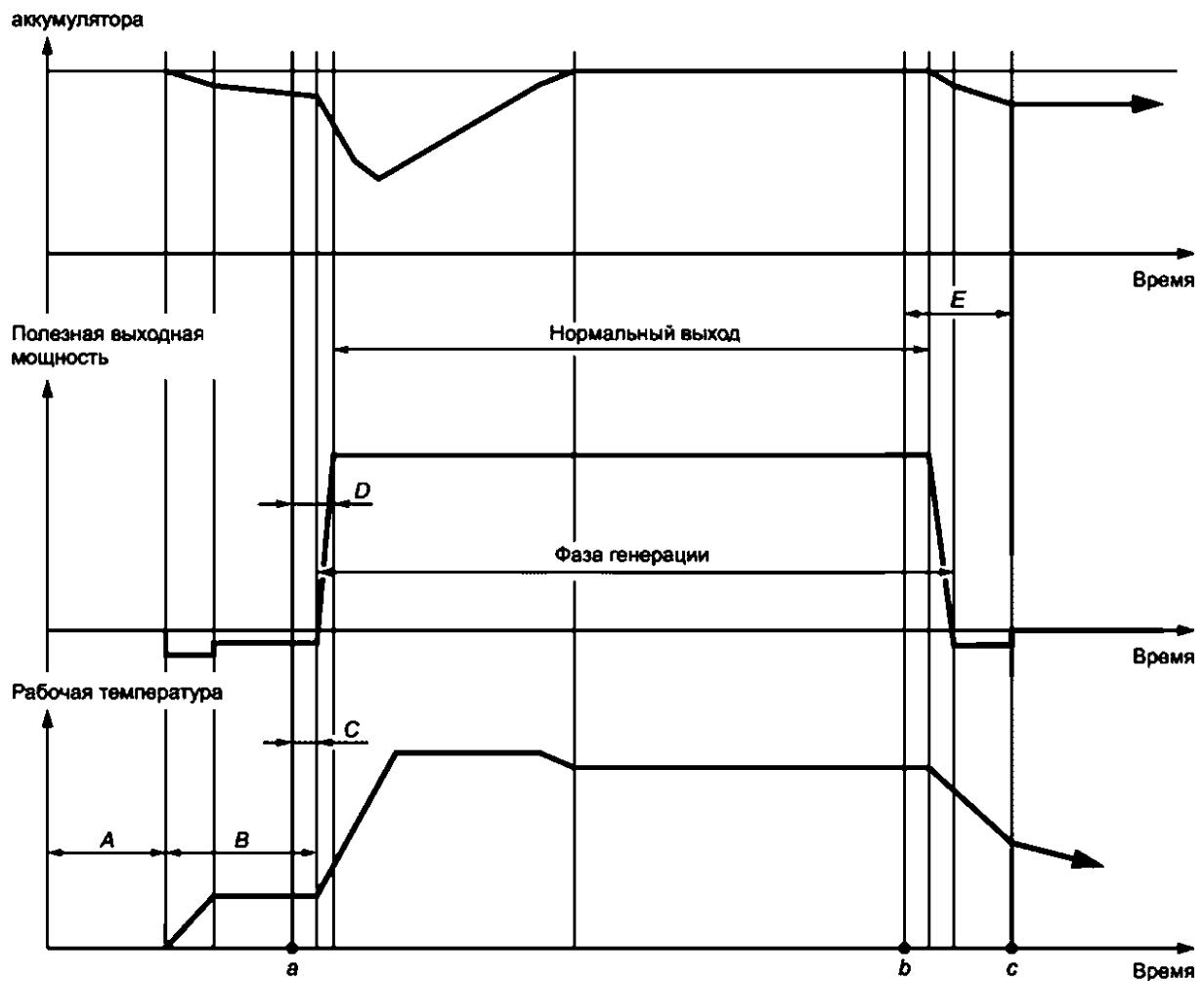
5

6 —

**13**



— ;  
 — ;  
 -1 — , ;  
 -2 — , ;  
 — , ;  
 — ;  
 F — , ;  
 b — ;  
 — ;  
 d — ( ( ) );  
 -1 -2 d — ( ( ) );  
 5 —

**14****I**

14.1

/

- (14.2);
- (14.3);
- (14.4);
- (14.5);
- (14.6);
- (14.7);

(14.4) (14.8).  
 (14.2), (14.3)  
 (14.9), (14.9.3)  
 (14.9.2), (14.9.4).

14.2

14.2.1  
14.2.1.1

50 %, 75 % /

(14.3) (14.4).  
14.2.1.2

a) 30

b) 30

c) (

50 75 % /

).

d) ( 3 ( )  
)

3 , ).

14.2.1.3  
14.2.1.3.1 $q_{vf0} \quad ^3/ , \quad q_{m1} \quad / .$ 1) :  $q_{vf} \quad ^3/$ 

$$q_{vf} = q_{jv}/A7; \quad (1)$$

:  $q_{vf} \quad ^3/ ;$   
 $q_{iv} \quad ^3/ ;$ — 2)  $q_{vf0} \quad ^3/$ 

$$q_{vf0} \quad ^3/$$
  

$$q_{vf} \quad ^3/ ;$$
  

$$Qvro = Qvf \quad ( / )^2 \quad <2>$$

$$: q_{vf0} \quad ^3/ ;$$
  

$$q_{vf} \quad ^3/ ;$$
  

$$t_0 \quad 288,15 \quad ;$$
  

$$tf \quad$$
  

$$p_f \quad 101,325 \quad ( . );$$
  

$$p_0 \quad ( . )$$

b)

$$q_{mf} /$$

$$Q_{mf} = Q_{imf}^7; \quad (3)$$

$$q_{mf} —$$

$$q_{imf} —$$

14.2.1.3.2

$$Q_{jnf} 8 /$$

a)

1)

$$\wedge, / ^3.$$

$$\wedge = / _0, \quad (4)$$

$$E_{fv} —$$

$$Q_{f0} —$$

$$Mq —$$

$$f_0 = 288,15 \text{ }, \quad 3/ \quad , \quad , \quad , \quad / ^3, \quad , \quad / ;$$

$$2,3645 \quad 10^{-2} \quad 3/ \quad ($$

$$Q_{ro} /$$

$$\begin{matrix} N \\ "X / /- \\ /=1 \end{matrix}$$

$$Q_{ro} —$$

$$j$$

$$f_0 / ;$$

$$j —$$

$$N —$$

$$;$$

$$;$$

1

ISO 6974, ISO 6975

.1.

2

(LHV).

HHV (

),

2)

$$Q_{inf}, / ,$$

$$Q_{nf} " 9vto ' EfV.$$

$$Q_{inf} —$$

$$g_{vf0} —$$

$$\wedge —$$

$$, / ;$$

$$, 3/ ;$$

$$/ ^3.$$

1 62282-3-200,

b)

1)

$$\text{EfM.} / .$$

$$\wedge_m = fOK > W_{mf}) - 1000. \quad (7)$$

$$E_{fm} —$$

$$Q_{f0} —$$

$$W_{mf} —$$

ASTM F2602.

» 14.2.1.3.2.

$$2) \quad Q_{inf} = \frac{Q_{nf}}{Q_{in}}, \quad (8)$$

$Q_{inf}$  — , ;  
 $E_{fm}$  — , ;  
 $q_{mf}$  — , / .  
 14.2.2  
 14.2.1

50, 75 % /

(14.3)  
 14.2.2.2  
 a)

30

b)

30

c)

(

50 75 %

/

d)

3 (

e)

20

f)

).  
 14.2.2.3

$E_{in}$

$$( = ( - ) Q_{fl}, \quad (9)$$

$E_{in}$  — , ;  
 — , ;  
 $Q_n$  — , / .  
 $Q_{inf}$  — / ,

$Q|nf=\wedge.$

( )

$Q_{inf}$  — , / ;  
 1 — , ;  
 7 — , .

1

(LHV).

HHV (

),

2

ASTM D4809-09

14.3

14.3.1

50, 75 % /

(14.2)

(14.4).

14.3.2

a)

30

b)

30

c)

50 75 %

/

d)

3

20

3

14.3.3

 $\Delta\Delta\Delta\Delta$ 

(11)

$VV_{out}$  —  
—  
— 7 —

14.4

14.4.1

50, 75 % /

(14.2)

(14.3).

14.4.2

30

a)

30

b)

c)

50 75 %

/

d)

60

## 14.4.3

20

3

a)

1)

 $q_{vr}$ 

$$Q_{vr} = Q_{ivhr}$$

02)

 $q_{vr}$   
 $q_{jvHR}$ 

2)

 $Q_{HR}$ 

$$\Delta HR = \Delta HR_1 \cdot HR_2 \cdot Q_{vr} \cdot P_{HR} \cdot S_{HR}$$

3)

 $Q_{hr}$   
 $f_{HR1}$ 
 $f_{HR2}$   
 $q_{vHR}$ 
 $P_{HR}$   
 $S_{HR}$ 
 $f_{HR1}$      $f_{HR2}$ 
 $f_{HR1}$ , / 3;

4,186    ~1    1.

b)

 $g_{mHR}$ , / ,

&lt;14)

 $q_{mHR}$   
 $q_{irnHR}$ 

1)

 $Q_{HR}$ , / ,

$$Q_{HR} = (HR_1 \cdot HR_2 \cdot mHR \cdot S_{HR})$$

5)

 $Q_{hr}$   
 $f_{HR1}$ 
 $f_{HR2}$   
 $q_{mHR}$ 
 $S_{HR}$   
 $f_{HR1}$ 

4,186    ~1    "1.

14.5

14.5.1

/

,

,

,

,

,

-

) 11.3.

14.5.2

:

,

(

,

)

) 11.3;

b)

,

 $\pm 2\%$ 

( 8).

14.5.3

a)

48

b)

,

8

48

c)

,

15

d)

e)

,

1

—

,

2

—

,

,

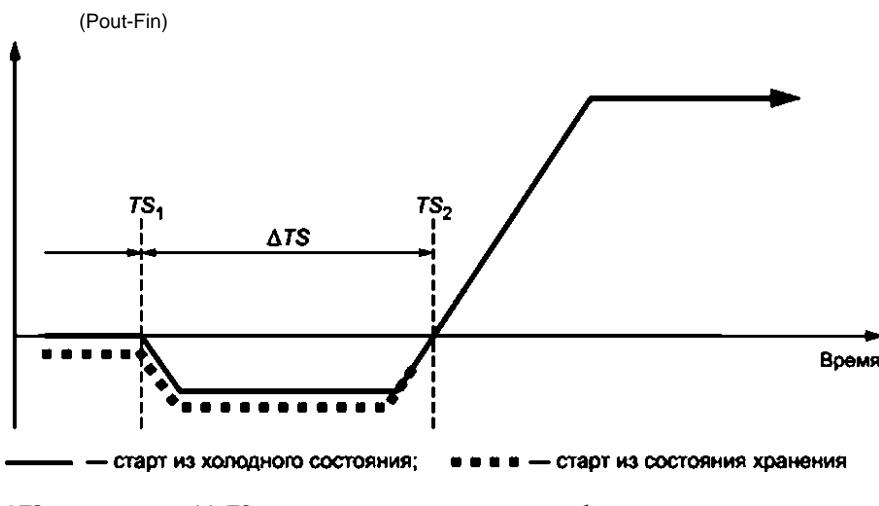
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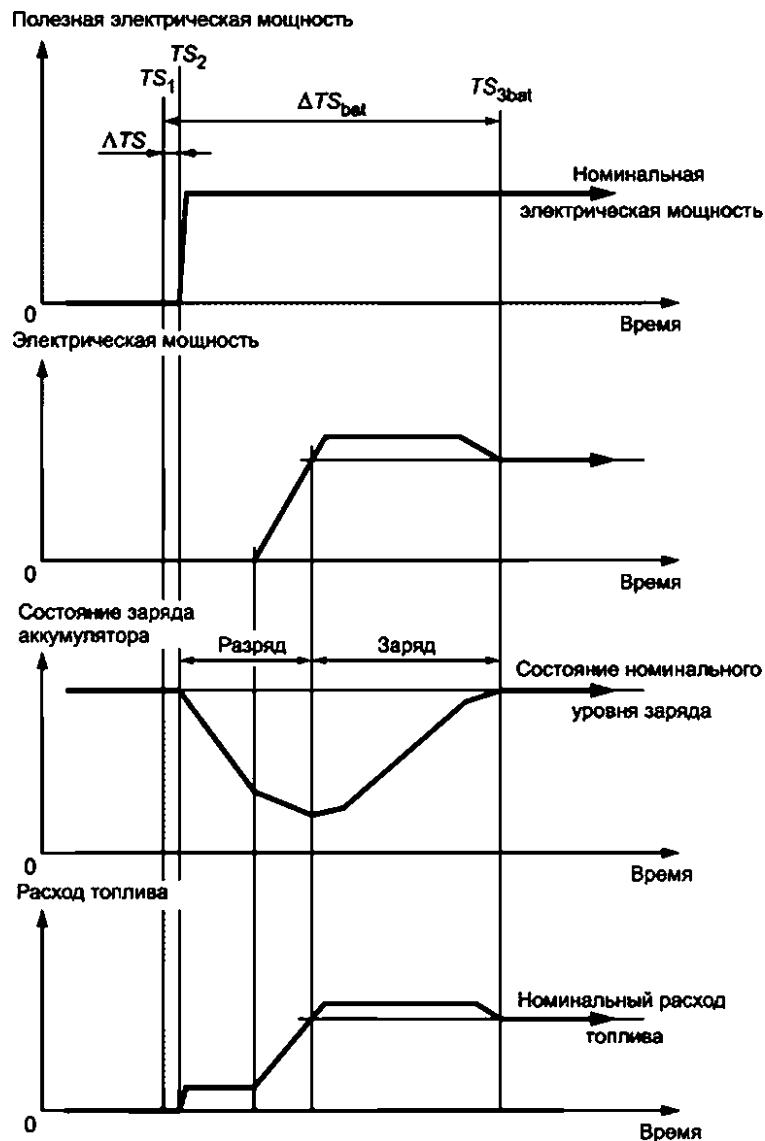
,

).

,



7 —

TSf —  
ATS —; TS<sub>2</sub> — ; TS<sup>at</sup> • ;

8 —

14.5.4  
14.5.4.1

( 7 8):

$$ATS = TS_2 - TS_1, \quad (16)$$

ATS —

, ;

TS —

;

TS<sub>2</sub> —

14.5.4.2

14.5.4.2.1

)

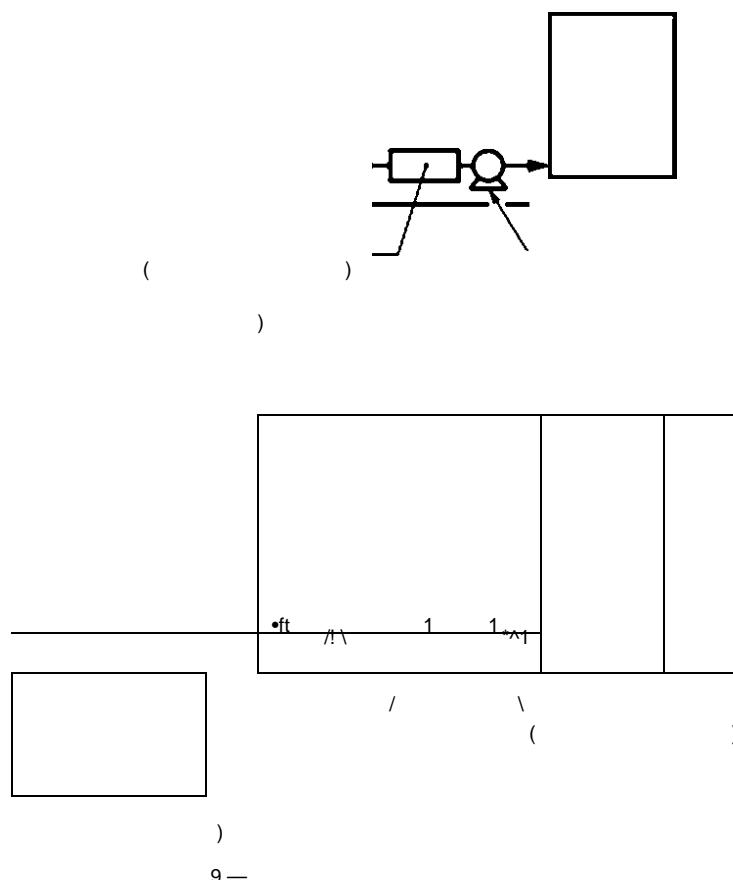
14.2.1.3.  
(1)-(8)],

14.2.1.3 [

14.2.1.3

14.2.2.3.

9,



$$\Delta_{\text{in startup bat}} = \frac{E_{\text{in}}}{W_{\text{out bat}}} \cdot TS_1 - TS_{\text{3t>at}} \cdot 3600 \cdot \%_{\text{utbat}} \cdot 100\% . \quad (17)$$

$f_{\text{in startup bat}} =$   
 $E_{\text{in}} =$   
 $TS_1 =$   
 $W_{\text{out bat}} =$   
 $\Delta_{\text{in startup bat}} =$   
 $TS_{\text{3t>at}} =$   
 $TS^{\wedge} =$   
 $, \% \text{ (14.9.2).}$

$$3600 \cdot W_{outbat} \cdot 100/ifo = kV_{outbat} \cdot E_{jn}$$

14.5.4.2.2  
a)

$$\wedge.nsortup = -W_{out}, \quad (18)$$

$$\begin{aligned} V^{\wedge}_{nstartU} p &= \\ 1 | &= TS, \quad ; \\ W_{out} &= TS. \quad . \\ b) & \end{aligned}$$

$$\wedge nstartupbat " \wedge nbat " \wedge outbab \quad 0 9)$$

$$\begin{aligned} V^{\wedge}_{nstartU} p_{bal} &= \\ TS_1 &= TS_{3bat}, \quad . \\ WJ_{nbat} &= TS, \quad . \\ W_{outbat} &= TS_1 \quad . \end{aligned}$$

14.6

14.6.1

14.6.2  
a)  
b)

14.6.3

3

$$instore----- \wedge 3600. \quad (20)$$

$$\begin{aligned} P_{jnstore} &= \\ instore &= \end{aligned}$$

14.7

14.7.1

## 14.7.2

a)

30

30

b)

1

c)

1

d)

e)

 $\pm 2\%$ 

1

h)

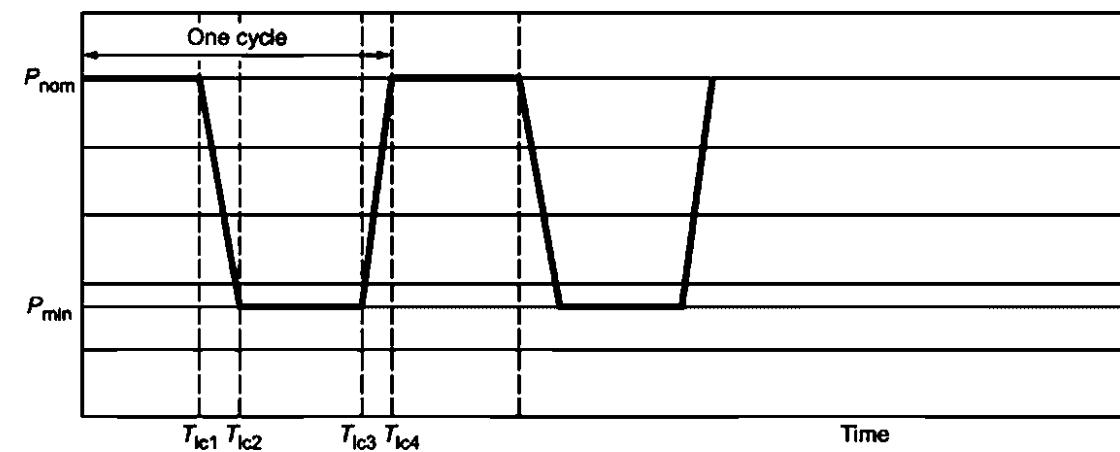
 $\pm 2\%$ 

i)

1

j)

d) i)



One cycle —

12%

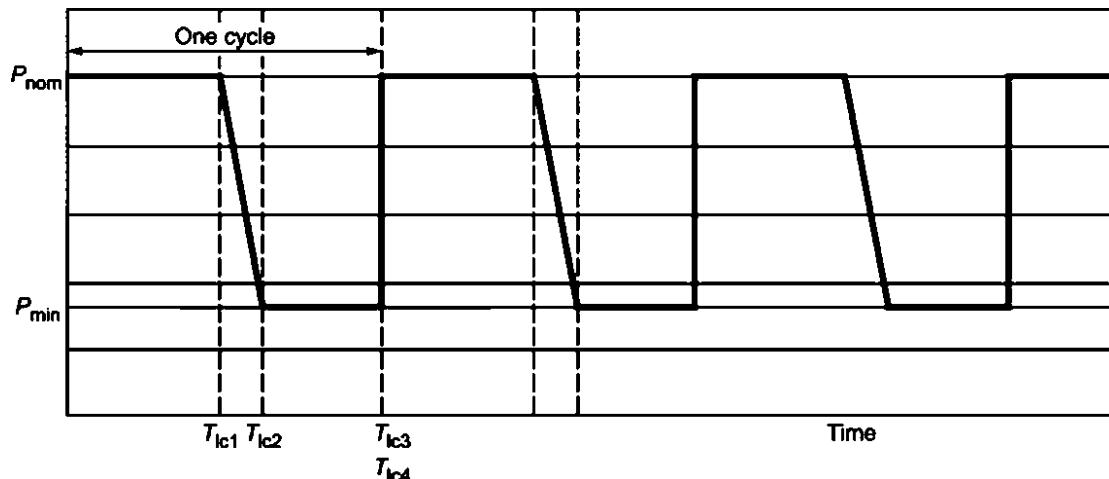
 $P_{min} \sim$ 

( 12);

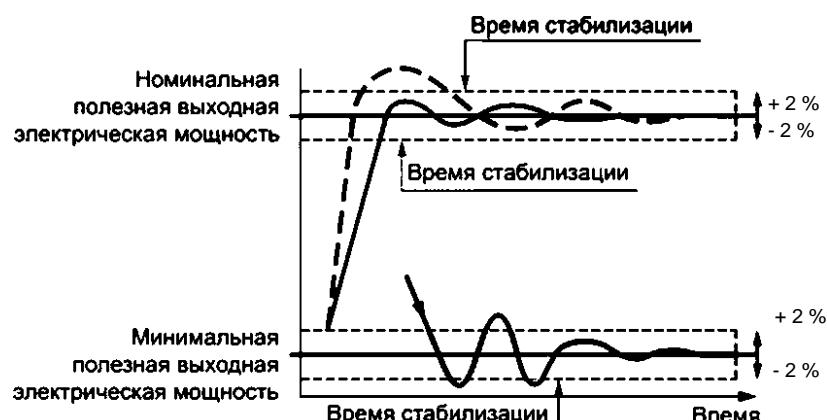
 $\wedge^* 2$  $\pm 2\%$ 

( 12);

10 —



One cycle —  
 $(\quad)$   $\pm 2\%$   
 $7|_1 \quad 7|_2$   
 $\wedge ic2 \quad , \quad (\quad) \quad \pm 2\%$   
 $11 \quad -$



12 —

## 14.7.3

$$\wedge d \wedge d' T ic dw rr \quad (21)$$

$$\wedge u = P d' 7 i c u p - \quad (22)$$

$PV_d$  —  
 $PV_U$  —  
 $P_d$  —  
 $A7j_{cdwn}$  —  
 $7|_1$  —  
 $, / ;$   
 $, / ;$   
 $P_{nom} \quad P_{min}, ;$   
 $7|_1 \quad 7|_2, ;$   
 $, .$

14.8

14.8.1

(2).

14.8.2

a)

30

b)

30

c)

(15),

15

d)

e)

1

2

150 %

).

14.8.3

14.8.3.1

(13)

$$bTE = TE_2 - TE_v$$

(23)

7 —

2 —

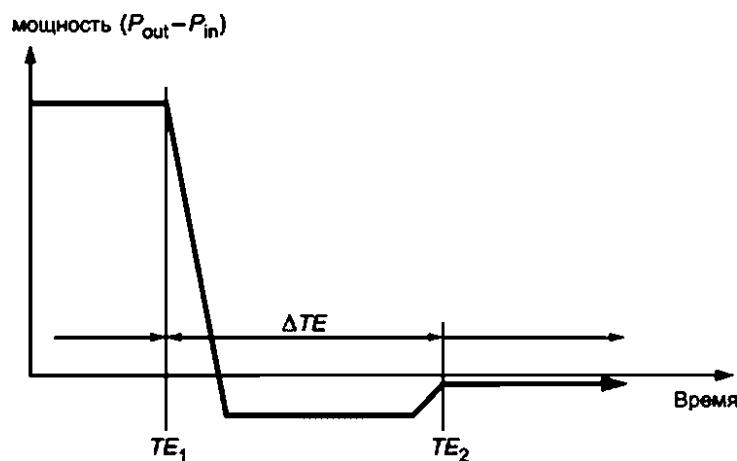
14.8.3.2

14.8.3.2.1

),

14.2.1.3,

(1)-(8),



— ; ; —  
? —

13 —

(9) (10)

9,

#### 14.8.3.2.2

$$\Delta_{\text{shutdown}} = \Delta n \% \text{ut.} \quad (24)$$

$W_{\text{shutdown}}$  —  
 $W_{\text{out}}$  —

VVJ<sub>n</sub> —

14.9

#### 14.9.1

14.9.2, 14.9.3 14.9.4.  
IEC 62282-3-200

IEC 62282-3-200.

## 14.9.2

, / . %.

$$\text{---} = \Delta - 100^{\circ}$$

$\frac{4nf}{\text{---}}$

&lt;25&gt;

—  
—  
 $Q_{jnf}$  —  
14.9.3

, %;  
, , (14.3.3);  
, / (14.2.1.3.2 14.2.2.3).

//<sub>th</sub> %,

$$\text{---} = \Delta$$

$\frac{4nf}{\text{---}}$

(26)

//<sub>th</sub> —  
 $Q_{Hr}$  —  
 $Q_{jnf}$  —

, %;  
, / (14.4.3);  
, / (14.2.1.3.2 14.2.2.3).

$f_{HR1}$        $f_{HR2}$ ,

## 14.9.4

%,

$$'/\text{total} = V_e *'/\text{th-}$$

&lt;27&gt;

—  
//<sub>(tota)</sub> —  
//<sub>(h)</sub> —

, %;  
, % (14.9.2);  
, % (14.9.3).

**15**

## 15.1

- (15.2);
- (15.3);
- (15.4).

## 15.2

## 15.2.1

; ; ; ; ( )

## 15.2.2

## 15.2.2.1

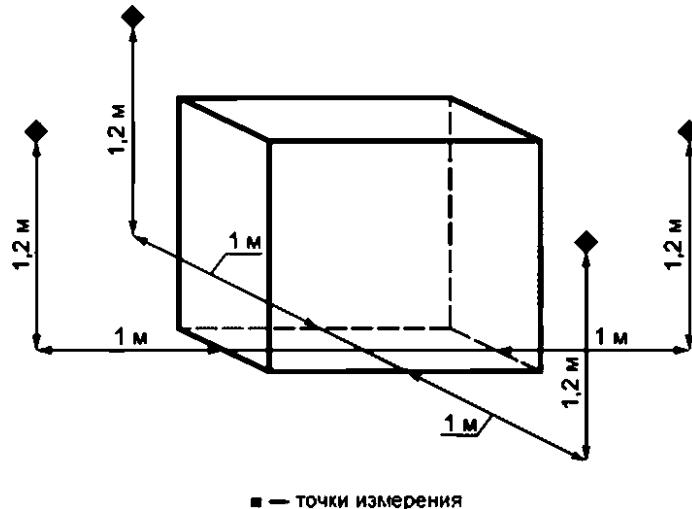
( , , , ) 50

1

## 15.2.2.2

ISO 6798.

1,2



14 —

## 5.2.2.3

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 , 10 , , , ,  
 3.

3 —

,	3	4	5	6	7	8	9
,	-3	-2			-1		

## 15.2.2.4

## 15.2.3

- a)
- b)
- c)

30

- d)

30

e)

f)

1  
46).

( , 45,7

)

15.2.4

a)

b)

15.2.2.3.

-

-

1

15.3

15.3.1

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15.3.3

a)

-

( )

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( )

( )

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( )

( )

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( )

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( )

b)

-

( )

,

,

( )

,

,

( )

,

,

( )

c)

d)

f)  
(ppm), % / 3

15  
15.3.4  
15.3.4.1

2

$$X_c = X_m O_{2t} / (O_{2t} - O_{2a}), \quad (28)$$

2  
15.3.4.2

a)  $v_f$ ,  $v_{ra}$

$$\nu_1 O = \nu_r \quad (\text{Pf/Po})' \quad (29)$$

$v_f$  — ;  
 $/_0$  — ;  
 $101,325$  ;  
 $f_f$  — ;  
 $p_f$  — ;  
b)  $q_f$

&lt;30&gt;

$Mq$  — ;  
 $M_{mf}$  — ;  
15.3.4.3

$$( = 12.011 + 1.00794 \quad a_p \quad (31)$$

$CH_{gf}$  — ;  
 $a_f$  — ;  
 $12,011$  — ;  
 $1.00794$  — ;

: 13,88 ( $\alpha_f = 1,85$ );  
: 13,97 ( $a_f = 1,94$ ).

15.3.4.4  
15.3.4.4.1

15.3.4.1, 15.3.4.2 15.3.4.3.

## 15.3.4.4.2

$$\text{CO}_{\text{mass}}, \frac{\text{CO}_{\text{dr}} 10^{14} + 10^{14}}{1 + 2, + \text{CO}_{\text{dr}} 10^{14} + 10^{14}}^{\frac{4}{4}} \quad (32)$$

$\text{CO}_{\text{mass}}$  —  
— 28,01 ( );  
 $\text{CH}_{\text{af}}$  — ;  
 $\text{CO}_{2\text{dr}}$  — . . %;  
 $\text{CO}_{\text{dr}}$  — , / <sup>3</sup> (ppm);  
 $7\text{HC}_{\text{dr}}$  — ( ), / <sup>3</sup>  
 $q_f$  — ;

## 15.3.4.4.3

$$\text{. } 7\text{HC}_{\text{mass}}, \frac{\text{CO}_{2\text{dr}} + \text{CO}_{\text{df}} 10^{14} + 7\text{HC}_{\text{d}}}{\text{CO}_{2\text{dr}} + \text{CO}_{\text{df}} 10^{14} + 7\text{HC}_{\text{d}}}^{\frac{1}{1}} \quad (33)$$

$7^*\text{HC}_{\text{mass}}$  — , / ;  
— ;  
( ) — ;  
 $\text{CO}_{2\text{dr}}$  — , . %;  
 $\text{CO}_{\text{dr}}$  — , / <sup>3</sup> (ppm);  
 $q_f$  — ( ), / <sup>3</sup>  
(ppm);

$$7 = 12,011 + 1,00794 \ll, \quad (34)$$

— ;  
 $\ll$  — ;  
12,011 — ;  
1,00794 — .

: 13,88 ( <sub>6</sub> = 1,85);  
: 13,97 (  $\ll$  = 1,94).

15.3.4.4.4  $\text{NO}_x$   
 $\text{NO}_x$

$\text{NO}_x$

$$\text{W}^{\text{xmass}} \sim \frac{\text{WOxdr IO}^{14}}{\text{CO}_{2\text{dr}} + \text{CO}_{\text{dr}} 10^{14} + \text{THC}_{\text{dr}}}^{\frac{4}{4}} \quad \text{Gf} \quad (35)$$

$\text{A/O}_{\text{mass}}$  —  
 $\text{NO}^{\text{a}}$  — 46,61 (  $\text{NO}_2$  );  
 $\text{CH}_{\text{af}}$  — ;  
 $\text{CO}_{2\text{dr}}$  — ;  
 $\text{CO}_{\text{dr}}$  — , . %;  
 $\text{NO}_{\text{xdr}}$  —  $\text{NO}_x$ , , / <sup>3</sup> (ppm);  
 $\text{THC}_{\text{df}}$  — ( ), / <sup>3</sup>  
 $q_f$  — , / .

## 15.3.4.4.5

$\frac{\text{SO}_2}{\text{SO}_2}$ ,  $\text{SO}_{2\text{mass}}$ ,

$$\text{SO} = \frac{\text{SO}_{2\text{M}}}{\text{CH}_{lt1} \text{CO}_{2\text{dr}} + \text{CO}_{\text{dr}}} \cdot \frac{\text{SO}_{2\text{dr}}}{10^4 + \text{THC}_{\text{dr}} \cdot 10^4} \cdot G, \quad (36)$$

$\text{SO}_{2\text{mass}}$ —  
 $\text{SO}_{2\text{M}}$ — 64,06 (

$\frac{\text{SO}_2}{\text{SO}_2}$ , / ;

$\text{CH}_{ai}$ —

$\text{CO}_{2\text{dr}}$ —

$\text{CO}_{\text{dr}}$ —

$\text{SO}_{2\text{dr}}$ —

$\text{TWC}_{\text{dr}}$ —

(ppm);

$q_f$ —

## 15.3.4.4.6

$\frac{\text{SO}_2}{\text{SO}_2}$ ,  $\text{CO}_{2\text{mass}}$ ,

$$\text{CO}_{2\text{mass}} = \frac{\text{CO}_{2\text{dr}}}{(\text{CO}_{2\text{dr}} - \text{CO}_{\text{dr}}) \cdot 10^4 + 7\text{HC}_{\text{dr}} \cdot 10^4} \cdot \frac{1252}{10^{-3}}, \quad (37)$$

$\text{CO}_{2\text{mass}}$ —  
 $\text{CO}_{2\text{dr}}$ — 44,01 (

$\frac{\text{CO}_2}{\text{CO}_2}$ , / ;

$\text{CH}_{ai}$ —

$\text{CO}_{2\text{dr}}$ —

$\text{CO}_{\text{dr}}$ —

$7\text{HC}_{\text{dr}}$ —

( );

$q_f$ —

## 15.3.4.5

## 15.3.4.5.1

## 15.3.4.1.

## 15.3.4.5.2

$$\text{CO}_{\text{conc}} = \text{CO}_{\text{dr}} \cdot 1252 \cdot 10^{-3}, \quad (38)$$

, /  $^3$ ;

$\text{CO}_{\text{dr}}$ —

## 15.3.4.5.3

, /  $^3$ .

$$\hat{\wedge} = \text{THC}_{\text{dr}} \cdot (0,537 + 0,045 \cdot \hat{\wedge}) \cdot 10^{-3}, \quad (39)$$

:  $\hat{\wedge}$ — , /  $^3$ ;

$7\text{HC}_{\text{dr}}$ —

);

$g$ —

: 1,85;

: 1,94.

15.3.4.5.4                   $\text{NO}_x$   
 $\text{NO}_x$ , , ,  $\text{NO}_x$   
 $\text{NO}_2:$   $WO_{\text{CO}_{\text{TC}}} = WO_{\text{CO}_{\text{dr}}} \cdot 2056 \cdot 10^{-3}$ , (40)

:  $\text{NO}_{\text{xconc}}$  —  $\text{NO}_x$ , /  $^3$ ;  
 $/V_{\text{O}_{\text{XDR}}}$  —  $\text{NO}_x$ , /  $^3$  (ppm).

15.3.4.5.5                   $\text{SO}_2$   
 $\text{SO}_2$   
 $\text{SO}_2 \text{conc} = \text{SO}_{2\text{dr}} \cdot 2863 \cdot 10^{-3}$ , (41)

$\text{SO}_{2\text{conc}}$  —  $\text{SO}_2$ , /  $^3$ ;  
 $\text{SO}_{2\text{dr}}$  —  $\text{SO}_2$ , /  $^3$  (ppm).

a)

b)

( 1 30 )

c)

15.3.4.7

15.3.4.8

15.3.4.9

15.4

15.4.1

## 15.4.2

a)

b)

c)

•

- pH;

-

•

ISO 6060 —

**16**

## 16.1

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 , ,  
 , 8 ,  
 , ,  
 / 14 15,

## 16.2

- a)
- b) ( , );
- c);
- d), ;
- e), ;
- f), ;
- g), ;
- h), ;
- i)

**16.3**

## 16.4

- a);
- b), ;
- c), ;
- d), ;
- e), ;
- f), ;
- g), ( . . );
- h)

( )

1 —

		, /	, /	/	,
1		802,69	891,56	50,035	55,574
2		1 428,84	1 562,14	47,52	51,95
3		2 043,37	2221,1	46,34	50,37
4	-	2 657,6	2 879,76	45,72	49,55
5	2-	2 648,42	2 870,58	45,57	49,39
6	-	3 272,00	3 538,6	45,35	49,04
7	2-	3 265,08	3 531,68	45,25	48,95
8	2.2-	3 250,83	3 517,43	45,06	48,75
9	-	3 887,21	4 198,24	45,11	48,72
10	2-	3 879,59	4 190,62	45,02	48,43
11	-	3 882,19	4 193,22	45,05	48,66
12	2.2-	3 869,8	4 180,83	44,91	48,51
13	2.3-	3 877,57	4 188,6	45,00	48,6
14	-	4 501,72	4 857,18	44,93	48,47
15	-	5 116,11	5 516,01	44,79	48,29
16	-	5 731,49	6 175,82	44,69	48,15
17	-	6 346,14	6 834,9	44,6	48,04
18		1 323,24	1 412,11	47,17	50,34
19		1 926,13	2 059,43	45,77	48,94
20	1-	2 540,97	2 718,7	45,29	48,46
21	-2-	2 534,2	2 711,9	45,17	48,33
22	-2-	2 530,5	2 708,3	45,1	48,27
23	2-	2 524,3	2 702,00	44,99	48,16
24	1-	3 155,59	3 377,75	44,99	48,16
25		1 855,09	1 943,96	46,3	48,52
26	1.2-	2 461,82	2 595,12	45,51	47,98
27	1.3-	2 408,8	2 542,1	44,53	47,00

1

		/	/	/	/
28		1 256,94	1 301,37	48,27	49,98
29		3 100,03	3 322,19	44,2	47,37
30		3 705,86	3 912,46	44,03	47,2
31		4 320,92	4 631,95	44,01	47,17
32		3 689,42	3 956,02	43,84	47,01
33		4 293,06	4 604,09	43,72	46,89
34		4 911,49	5 266,95	43,77	46,94
35		3 169,56	3 302,86	40,58	42,28
36		3 772,08	3 949,81	40,94	42,87
37		4 387,37	4 609,53	41,33	43,42
38	-	4 376,48	4 598,64	41,22	43,31
39		676,22	765,09	21,1	23,88
40		1 151,41	1 240,28	23,93	25,78
41		241,72	286,15	119,91	141,95
42		0	44,433	0	2,47
43		517,95	562,38	15,2	16,5
44		316,86	383,51	18,61	22,52
45		649,5	671,7	24,03	24,85
46		282,91	282,91	,1	10,1
47		548,15	548,15	9,12	9,12
48		1 104,32	1 104,32	14,5	14,5

—

3 4 ISO6976:1995.

( )<sup>8</sup>

81.

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	1	025	61	82	G30	1	D1	02	81	62	F1	F2	N1	N2	N4	N6	4	31	32	J3	J4	02			
,	2	67.2	86.0	63.0	814	100.0065.1	740	75.8	872	88.0	71.7	810	85.7	00.65	80.50	90.35	8937	90.00	89.6	88.9	873	89.2	83.4		
>	5.0	1.7	0.0	11.7	0.0	0.0	8.3	.	11.7	0.0	10.0	15.0	1.7	13.3	4.0	4.0	4.0	5.0	6.0	5.6	6.8	5.9	4.5	6.7	
CjH <sub>8</sub>	0.7	3.3	0.0	10	0.0	0.0	4.0	3.3	0.7	13	0.0	2.7	8.0	0.7	1.0	1.0	1.0	1.0	1.0	3.4	3.1	5.3	2.7	4.7	
C«H,o	02	0.0	0.0	0.0	1.0	0.0	0.7	1.0	0.5	02	0.0	0.3	0.2	0.2	-0.3	-03	-0.15	-0.3	-0.2	1.4	1.2	1.2	3.4	13	
5 ))}														1*0.3		2							1.3		
.	0.1	0.0	0.0	0.0	0.7	0.0	0.6	0.4	03	0.1	0.0	0.2	0.1	0.1	-0.1	-0.15	-0.15	-0.1	-0.2	0.0	0.0	0.0	0.0	1.0	
.	0.1	0.0	0.0	0.0	0.3	0.0	03	0.3	03	0.1	0.0	0.1	0.1	0.1	0.05	0.1	0.1	0.03	0.2	0.0	0.0	0.0	0.0	0.4	
#	.	10.0	0.0	5.6	2.2	0.0	5.6	1.1	83	1.1	1.1	.	0.0	0.0	1.0		1.0	1.0	0.8	0.0	0.0	0.0	0.0	2.2	
N?	20.0	17.6	14.0	17	13.3	0.0	15.6	15.6	22	0.0	0.0	6.7	0.0	0.0	23	15	2.5	23	1.2	0.0	0.0	0.1	.1	22	
LHV.	734	7.86	8.13	8.60	0.01	0.45	8.66	8.58	1011	10.18	10.65	10.77	11.10	1126	1028	10.33	10.33	1038	10.66	1129	11.28	11.56	1138	11.92	
LHV.	2821	26.30	29.25	3101	32.43	34.02	34.77	34.48	36.76	36.68	38.34	38.77	40.30	40.55	37.01	37.18	37.18	37.18	37.37	38.37	40.64	40.66	41.83	41.69	
HKV.	.	6.71	9.03	0.84	0.00	10.40	10.67	10.80	1130	11.31	11.81	11.00	1138	>2.47	11.15	11.20	11.07	1125	11.56	12.51	1231	1180	12.82	13,17	13.20
HKV.	312?	31.38	32.40	38.41	35.06	37.78	38.40	38.14	40.67	40.72	42.51	42.85	44.00	44.90	40.12	40.32	39.85	40.52	41.80	45.02	45.03	46.07	46.15	47.42	47.50

	JP1	1A	1B	1C	10	1E	2A	28	2C	2D	38	3C	30	IF	3G	3H	G3O		
=4 <sup>M</sup> tO	0.8 980 1.2	0.0 100.0 0.0	5.0 90.0 5.0	0.0 900 100	5.0 800 15.0	0.0 80.0 20.0	5.0 70.0 25.0	0.0 70.0 0.0	50 600 35.0	0.0 60.0 40.0	5.0 50.0 45.0	0.0 50.0 50.0	5.0 40.0 55.0	0.0 40.0 60.0	5.0 20.0 78.0	0.0 20.0 80.0	5.0 0.0 98.0	0.0 0.0 1000	
.HV. kBt mj M' .HV. MQx<hP	2837 91.35	25.94 93.38	25.98 93.47	28.60 96.48	28.62 96.55	27.65 99.S4	27.68 99.63	28.51 102.82	28.53 102.71	2938 105.70	2938 105.78	30.22 106.77	3024 108.86	31.07 11185	31.95 115.02	32.78 118.01	33.68 121.17	34.49 124.16	32.25 118.09
iHV. HHV	' * 27.58 99.22	28.22 101.58	28.25 101.69	29.14 104.90	29.14 105.00	30.08 106.21	30.09 108.31	30.98 111.32	31.00 111.82	31.90 114.83	31.92 114.92	32.82 118.13	32.84 118.23	33.73 121.44	34.68 124.85	35.S7 127.06	38.52 131.47	37.41 134.68	34.94 125.81

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1	-		14.6	
2		-	14.5	
3			14.2 14.3 144	
4		75 % -	14.2 14.3 144	
5		50 % -	14.2 14.3 144	
6			14.2 14.3 144	
7		,	14.8	
6	-	, - ,	14.7	8
9			15.2	30
10	.	- -	15.2 15.3 15.4	
11	.		15.2 15.3 154	1
12	.		15.2 15.3 15.4	

( )

D.1.

D.1 —

		NOx	SO <sub>2</sub>	

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16.2.

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a),  
b),  
c),  
d),  
e)
  
  
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a),  
b),  
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2),  
3),  
4),  
5)

( )

IEC 61672-1	—	*
IEC 62282-3-200	—	
ISO 5815	—	*
ISO 6060	—	
ISO 6798	—	*
ISO 9000	IDT	ISO 9000—2011 « »
ASTM F2602	—	*
* — : IDT —		

## IEC 62282-3-201—2015

- [1] IEC 60050-601:1985 International Electrotechnical Vocabulary — Part 601: Generation, transmission and distribution of electricity — General (601: )
- [2] IEC 61672-2 Electroacoustic — Sound level meters — Part 2: Pattern evaluation tests (2. )
- [3] IEC/TS 62282-1:2010 Fuel cell technologies — Part 1: Terminology ( )
- [4] ISO 6326 (all parts) Natural gas - Determination of sulfur compounds ( )
- [5] ISO 6974 (all parts) Natural gas - Determination of composition with defined uncertainty by gas chromatography ( )
- [6] ISO 6975 (all parts) Natural gas - Extended analysis — Gas chromatographic method ( )
- [7] ISO 6976 Natural gas — Calculation of calorific values, density, relative density and Wobbe index from composition ( )
- [8] ISO 7934 Stationary source emissions — Determination of the mass concentration of sulfur dioxide — Hydrogen peroxide/barium perchlorate/Thorin method ( )
- [9] ISO 7935 Stationary source emissions — Determination of the mass concentration of sulfur dioxide — Performance characteristics of automated measuring methods ( )
- [ ] ISO 7941 Commercial propane and butane — Analysis by gas chromatography ( )
- [11] ISO 10396 Stationary source emissions — Sampling for the automated determination of gas concentrations for permanently installed monitoring systems ( )
- [12] ISO 10849 Stationary source emissions — Determination of the mass concentration of nitrogen oxides — Performance characteristics of automated measuring systems ( )
- [13] ISO 11042-1 Gas turbines — Exhaust gas emission — Part 1: Measurement and evaluation (1. )
- [14] ISO 11042-2 Gas turbines — Exhaust gas emission — Part 2: Automated emission monitoring (2. )
- [15] ISO 11541 Natural gas — Determination of water content at high pressure ( )
- [16] ISO 11564 Stationary source emissions — Determination of the mass concentration of nitrogen oxides — Naphthylethylenediamine photometric method ( )
- [17] ISO/TR 15916 Basic consideration for the safety of hydrogen systems ( )
- [18] SAE ARP1533A-2004 Procedure for the Analysis and Evaluation of Gaseous Emissions from Aircraft Engines ( )
- [19] EN 50465 EN 50465 Gas appliances — Fuel cell gas heating appliances — Fuel cell gas heating appliance of nominal heat input inferior or equal to 70 kW ( )
- [20] ASTM D4809-09 Standard Test Method for Heat of Combustion of Liquid Hydrocarbon Fuels by Bomb Calorimeter (Precision Method) (70 )

620.93:006.354

27.070

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