

**5817-
2021**

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**(ISO 5817:2014, Welding — Fusion-welded joints in steel, nickel, titanium
and their alloys (beam welding excluded) — Quality levels, IDT)**



2021

5817—2021

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4 5617:2014 « .

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) . » (ISO 5817:2014 «Welding — Fusion-welded joints

in steel, nickel, titanium and their alloys (beam welding excluded) — Quality levels for imperfections». IDT).

ISO/TC 44 «

», SC 10 « .

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29 2015 . Nt 162- « 26 *

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(www.gost.ru)

© ISO. 2014 —

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5817—2021

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Welding. Fuski-welded joints in steel, nickel, titanium and their alloys (beam welding excluded). Quality levels

— 2021—09—01

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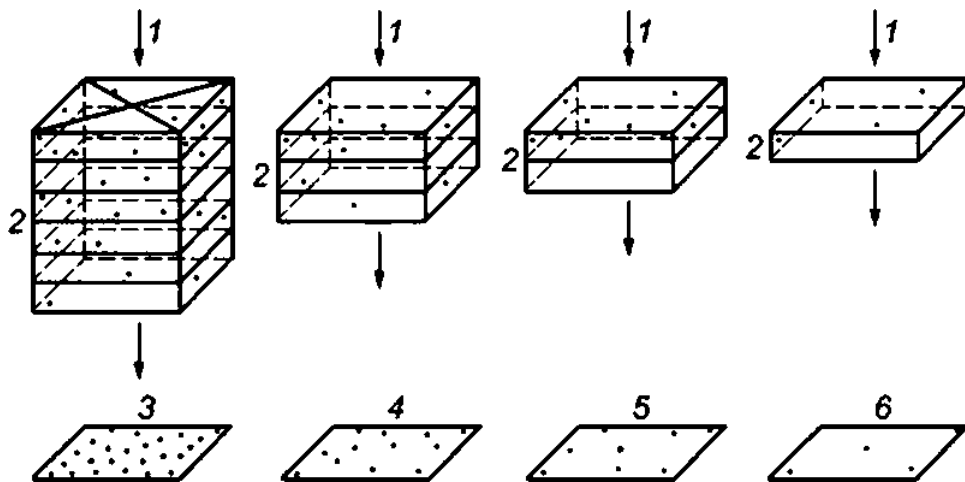
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5817—2021

ISO 6520*1:2007, Welding and allied processes — Classification of geometric imperfections in metallic materials — Part 1: Fusion welding. (

	1.)	
3			:
3.1	(quality level):	,	
3.2	(fitness*for*purpose):	,	
3.3	(short imperfections):	,	25
100-	100	,	
3.4	(short imperfections):	,	25 %
	100	.	
3.5	(systematic imperfections):	,	
3.6	(projected area):	,	
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		(. 1).	
3.7	(cross-sectional area):	,	
3.8	(smooth weld transition):		
3.9	(FATx) (fatigue class):		S— N. —
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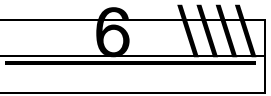
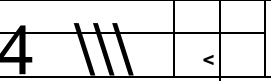
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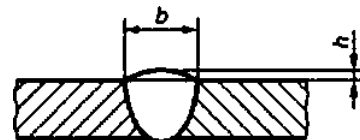
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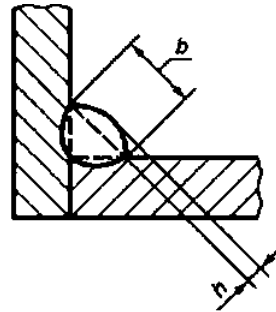


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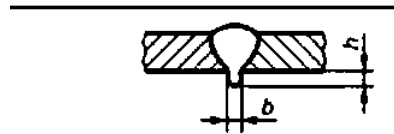
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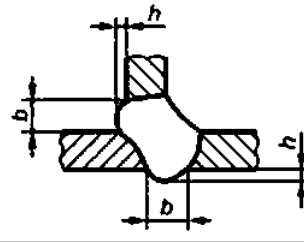


<i>l</i>	D				
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1.11 504



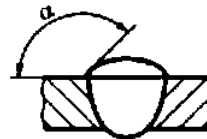
0,5 — 3	s 1	* 0.6 6:	« 1	+ 0.3 ft	5 1	+0.1 '.
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Стыковые швы

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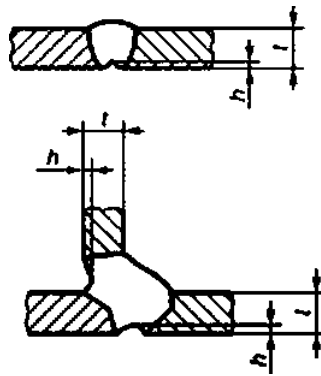
	505	/ -				«2100*	«2110*
1.13	506		20.5	<i>hs0,2b</i>			
1.14	509		0,5—3		:	:	
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1.15	510		20.5		:	:	:
1.16	512	,	20.5		<i>h S</i> 0.25 f, 2	<i>ft</i> £ 0.11. 1	<i>h</i> £ 0,051. 0.5
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6520-1

1.17 515



l.

0.5—3 ft S 0.2 +0,11

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h \$0.1 *t*

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/15 0,2*l.*
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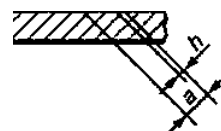
1.20 5213

0.5-3

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1.21	5214			20.5		<i>h-s</i> 1 *0.2 , 4	AS1 *0.15 . 3
1.22	601			20.5	,		
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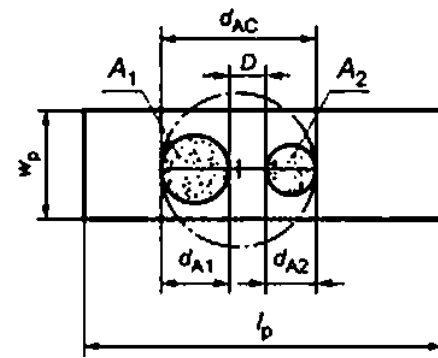
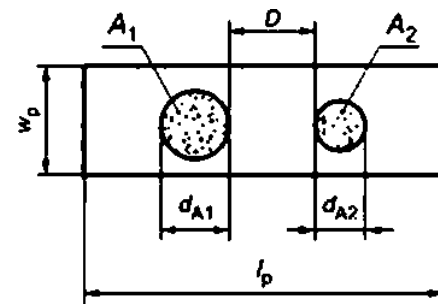
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2.2	1001		(50)	20.5		очHosioro	-
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			- ;		5 ;	4 ;	;
			-		ds 0.4 ,	ds0.3a.No	0\$ 02 ,
					5	4	

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2013



$l = 100$

d_A

$$d_{A1} \wedge d_{A2} \cdot D$$

D		
$\wedge 25$ d. *)	$d_A \leq 20$	$d_A \leq 15$ 3. $wJ\tilde{r}$

1

	6520-1			1.	0		
2.4	2013		d_A , d_{A1} d_{A2} d^{\wedge} -				
2.5	2014			.5	ft £0.4 . 4 /s . 75	ft S 0.3 8. 3 /\$ s. 50	ft £0.2 8. 2 /£ . 25
				20.5	ft£0.4a. 4 (£ . 75	ft£0.3a. 3 /£ . 50	ft £02 . 2 /s . 25
			1 (D > d [^]) /				
			D				
			>	J			
			2 (D < d ₂) /				
			3				
			>0				
			= 100 . 1: d _t = ft. 2: d, d ₂ = ft				

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	6520-1			1.			
					0		
2.6	2015			20.5	h £ 0.4 \$. 4 ; / £ . 75	£ 0.38. 3 ; /£8. 50	£0.2 8. 2 ; /£8. 25
	2016			20.5	£0.4 . 4 ; /£ . 75	/ £0.3 , 3 ; /£ . 50	£02 . 2 ; /£ . 25
2.7	202			20.5	we - , - - : : : £0.4 8. 4 ; : h £0.4 . 4		
2.8	2024			0,5-3 >3	h /£ 0,2 /; /£ 0,2 /, 2		
			h /				
2.9	300			20,5	£ 0.4 8. 4 ; / £ . 75	£ 0.3 8. 3 ; 1 £ 8. 50	£0.2 8. 2 ; /£8. 25

£

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«520-1
2.9 301
302
303

2.10 304

2.11 3042

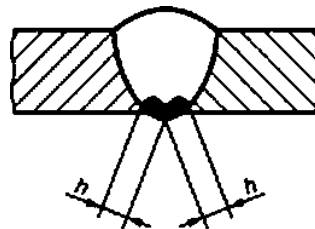
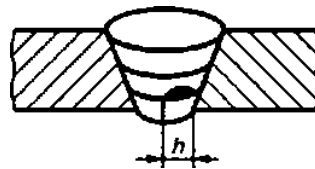
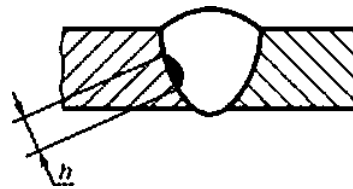
2.12 401

4011

4012

4013

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D
\$0,4 , 4 ; \$0,3 . 3 : \$02 . 2 :
/\$, 75 /\$, 50 /s . 25

20.5 \$0.4 \$. \$0.2\$.
2

0.5 \$0.4 . 4 \$0.3 , 3 \$0.2 . 2

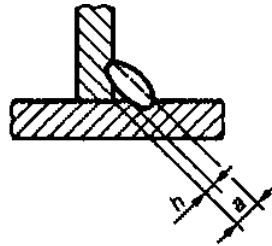
20.5

20.5

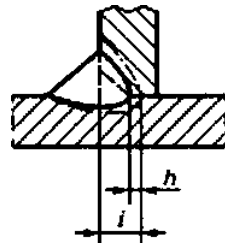
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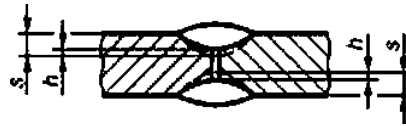
2.13 402



Т-образное соединение (угловой шов)



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2 ft s 0.1 /.
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	ft \$ 0.25 t. 5	ft \$0.151. 4	ft \$ 0.11.
	£0.5	ft \$ 0.51, 4	ft \$ 0.51, 2

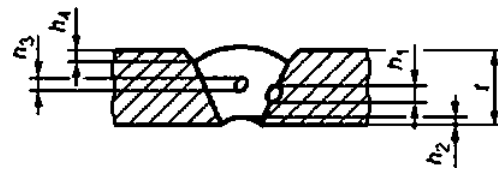
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3.2	617		00	KOMt	0.5-3 >3	0	\$0.5 + 0.1 £ 1 0.3 4	£ 0.3 +0.1 £0,5 +0.2	£0.2 +0.1 £0.5 + 0.1 2

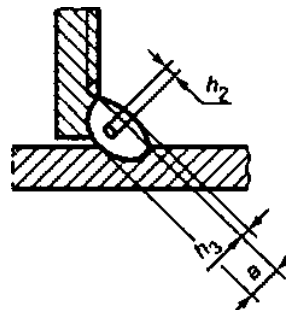
4

4.1



$$| + /ij^* + h_t =$$

..



$$| + 3^* =$$

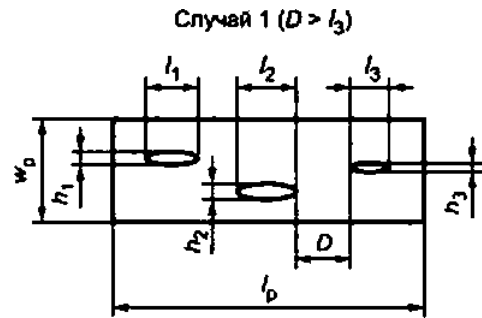
0.5-3

> 3

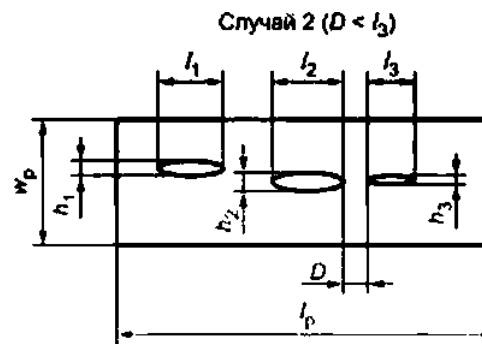
£ 0.4 £025	£03 £0.2	£ 0.2 £0.15	

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«520-1



$$r_{ij} = l_2 \quad 3 \cdot l_3 \cdot l$$



$$l_1 \cdot l_1 + l_2 \cdot l_2 + \frac{h_2 + h_3}{2} \cdot D + l_3 \cdot l_3 = \Sigma h \cdot l$$

1 " /
 « (1).
 D ,
 (2).

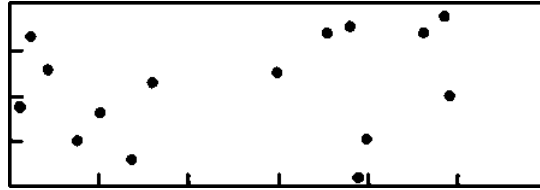
0		
<i>lh</i> IS 16 %	£ /«8%	Lh-/S4 %

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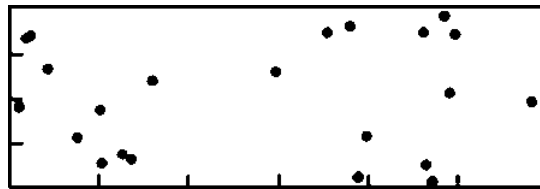
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.1— .9

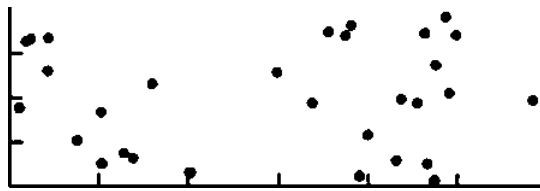
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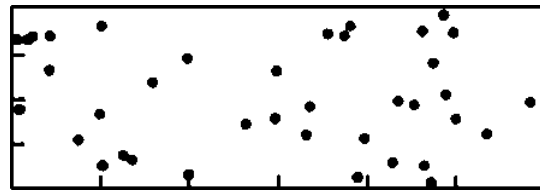
.1 — 1% .15 = 1 uu



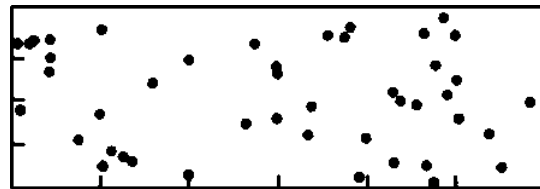
.2 — 1.5% .23 = 1



. — 2% .30 , d = 1

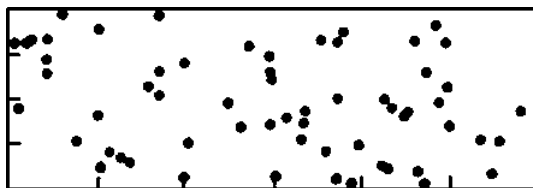


.4 — 2.5% .38 , d = 1

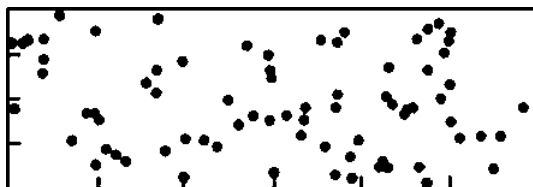


.5 — 3% .45 , d = 1

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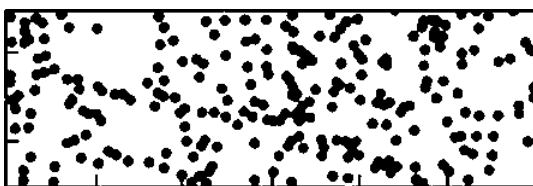
.6 — 4% .61 , $d = 1$



.7 — 5% .76 , $d = 1$



.8 — 8% .122 , $d = 1$



.9 — 16% .244 , $d = 1$

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0.5

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(FAT — fatigue class).
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125 — FAT 125 .

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 2— S817-B90
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					*	B125
1.5	401		2 0.5		3	a
1.7	5011 5012		>3	3	3	He
1.8	5013		>3		3	He
1.9	502	()	2 0.5		3	hi 0,2 + 0.1 b. 2
1.10	503	()	2 0.5		3	
1.11	504		0,5—3		3	h S 0.2 + 0.05 b
			>3		3	h \$ 0.2 + 0.05 b. 1
1.12	505		2 0.5		3	a
	5052	5052	2 0.5			2 4
1.14	509 511		>3	3	3	
1.16	512	()	2 0.5	3	3	
1.17	515		>3	3	3	
1.23	602		2 0.5	3	3	
2.3	2011 2012		2 0.5	3	3	: \$ 1 % - : S 2 % dS0.1 s. 1
2.4	2013		2 0.5	3	S3% ^d dSO.2 s. dSO.2 a. d\$2.5 mm	S2% ^d dSO.1 s. 0.5

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. 1

Nt	6520-1		t.			
				C63 ^e	90	125
2.5	2014		2 0.5			: s 1 % ^d - : s 2 % ^d d s 0.1 s. 1
2.6	2015 2016		2 0.5		hi 0.2 s 0.2 . /1 2 : 1 2.5 : - : 1S 20	
2.9	300 301 302		2 0.5		h s 0.2 s 0.2 . /1 2 : t 2.5 - : 1S 20	
3.1	5071		2 0.5		h £ 0.1 /. 3	h £ 0,05 /. 1.5
	5072		2 0.5		h \$ 0.5 /. 1	
3.3	508	6	2 0.5	OS2*	psr	psi*

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- IDT —

5817—2021

- [1] ISO 17635. Non-destructive testing of welds — General rules for metallic materials ()
- [2] ISO 2553, Welding and allied processes — Symbolic representation on drawings — Welded, brazed and soldered joints ()
- [3] ISO 4063, Welding and allied processes — Nomenclature of processes and reference numbers ()
- [4] ISO 13919-1. Welding — Electron and laser-beam welded joints — Guidance on quality levels for imperfections — Part 1: Steel ()
- [5] HW-Catalogue. Reference radiographs for the assessment of weld imperfections in accordance with ISO 5817. OVS Media Verlag. Dusseldorf
- [6] Hobbacher A. ed. Recommendations for fatigue design of welded joints and components HW document XIII-1823-0. Welding Research Council New York. WRC-BJletn 520. 2009
- [7] Hobbacher A. & Kassner M On Relation between Fatigue Properties of Welded Joints. Quality Criteria and Groups in ISO 5817. IIW-document XIII-2323-10
- [8] Karlsson N.. & Lenander P.H. Analysis of fatigue life in two weld class systems. Master thesis in Solid Mechanics. LITH-IKP-EX-05/2302-SE. Linköping University. Sweden. 2005

5817—2021

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17.06.2021

24.06.2021

60*84%

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